

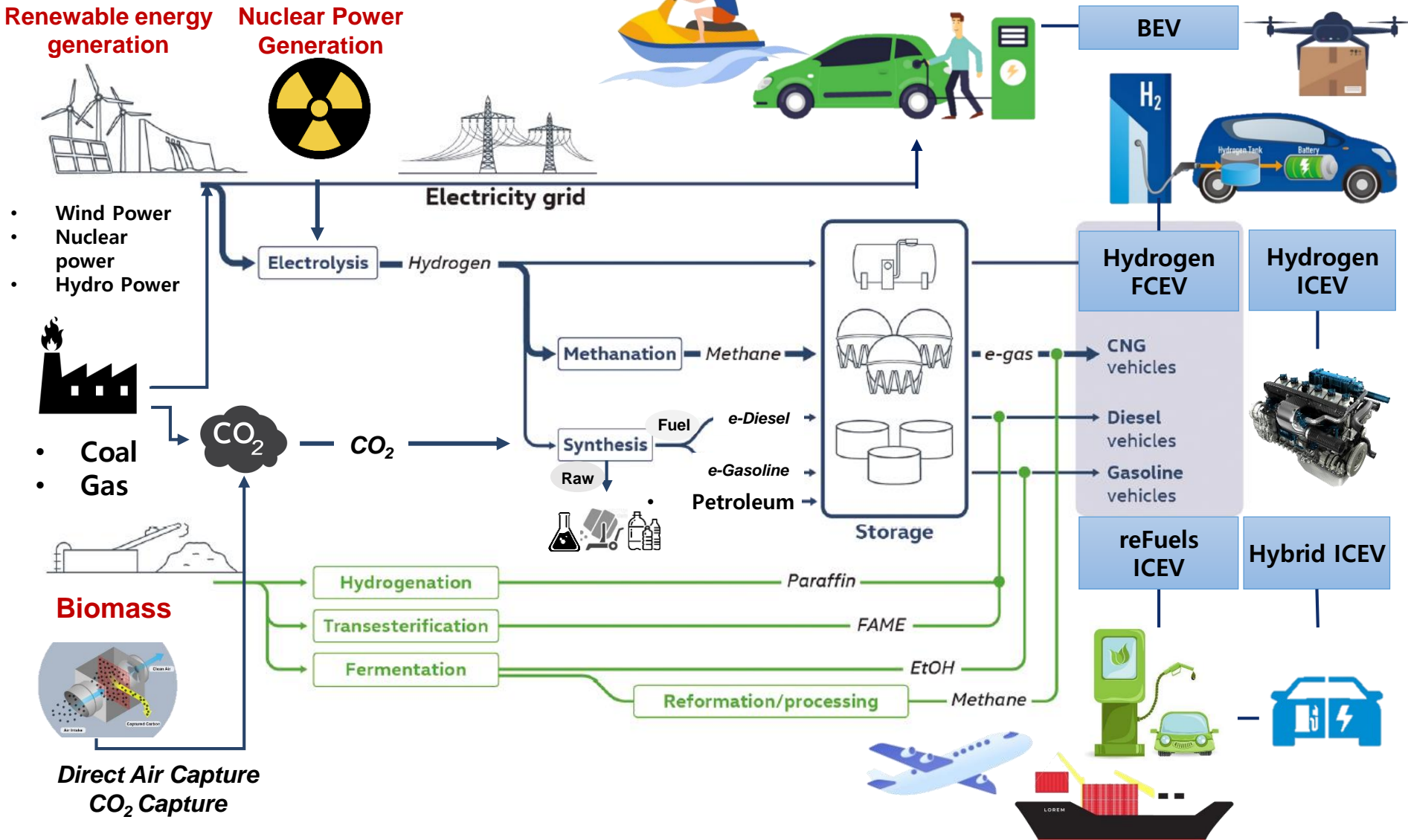
Lean Stratified Charged Hydrogen Combustion and Pollutant Formation



13 December 2023
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Active Carbon Neutrality (Reduction) Transport Power



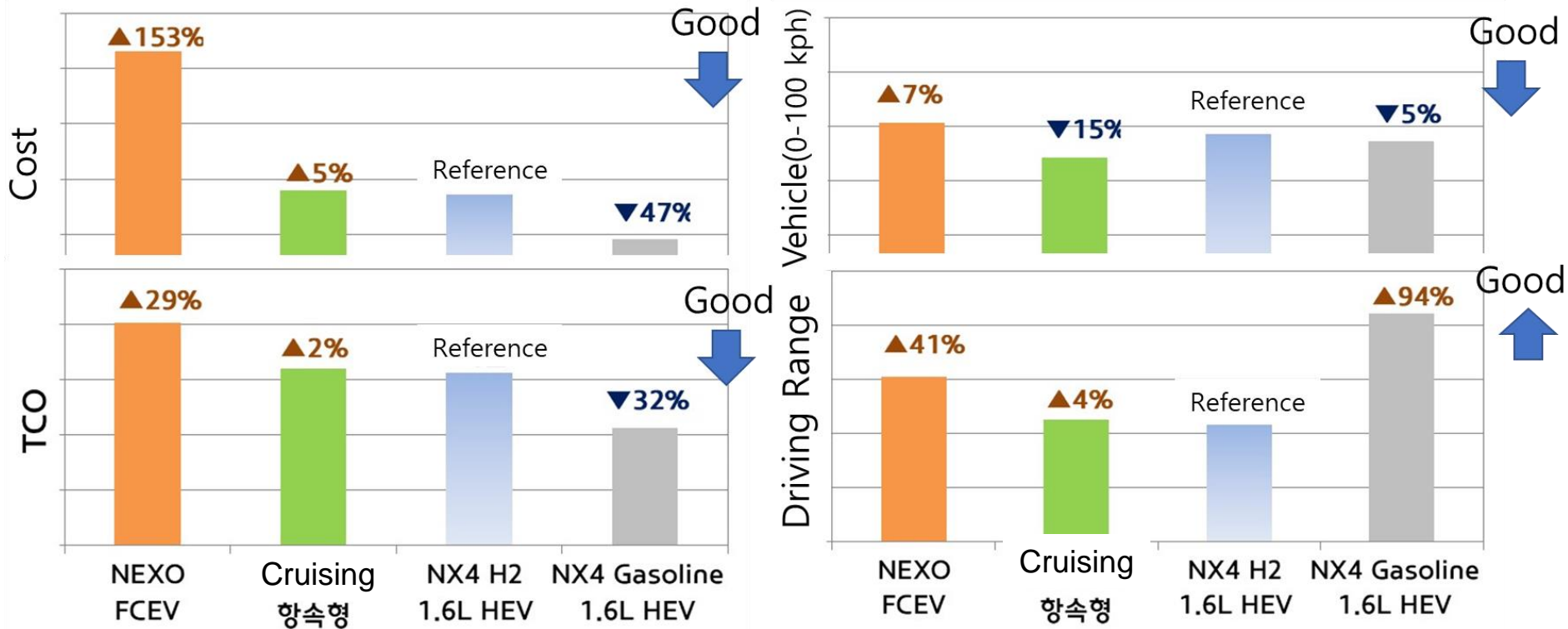
reFuel = Carbon-neutral fuel = Carbonless fuel+Bio-fuel+e-fuel

Source: Vienna motor symposium, 2018

Source: Position paper, IASTEC, 2021

Hydrogen Engine Competitiveness

- Competitive H2 ICE in aspect of value for money (5% ↑ over BEV, 153% ↑ over FCEV)
- Driving range 4% disadvantage over BEV, 41% disadvantage over FCEV
- Need to maximize H2 engine efficiency and develop innovative technology for H2 fuel tank
- H2ICE allows more sustainable supply chain independent from rare earth material needed for BEV & FCEV



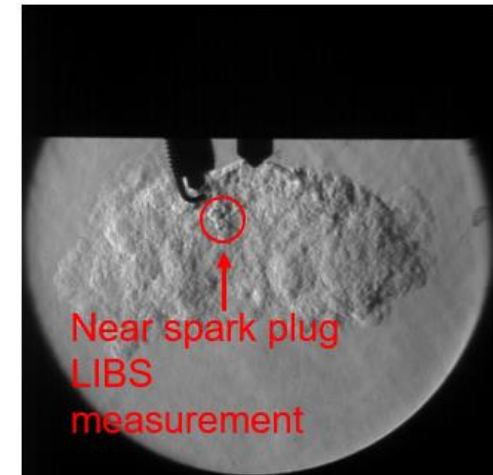
Source: R&D Technology Forum : Sustainable Carbon neutral ICE, Hyundai Motor Company, 2023

1. Mixture formation with hydrogen injection in a constant-volume chamber
 - Visualization of mixing process with Schlieren
 - *LIBS measurement on hydrogen-nitrogen mixture strength
 - OH Chemiluminescence on hydrogen combustion with single injection
 - Characterization of double hydrogen injection

2. Lean stratified charge combustion in a hydrogen engine
 - Combustion stability and NOx emission measurement in single-cylinder engine
 - Effects of EGR and post-injection on NOx emission reduction in prototype multi-cylinder engine

* LIBS = Laser - Induced Breakdown Spectroscopy

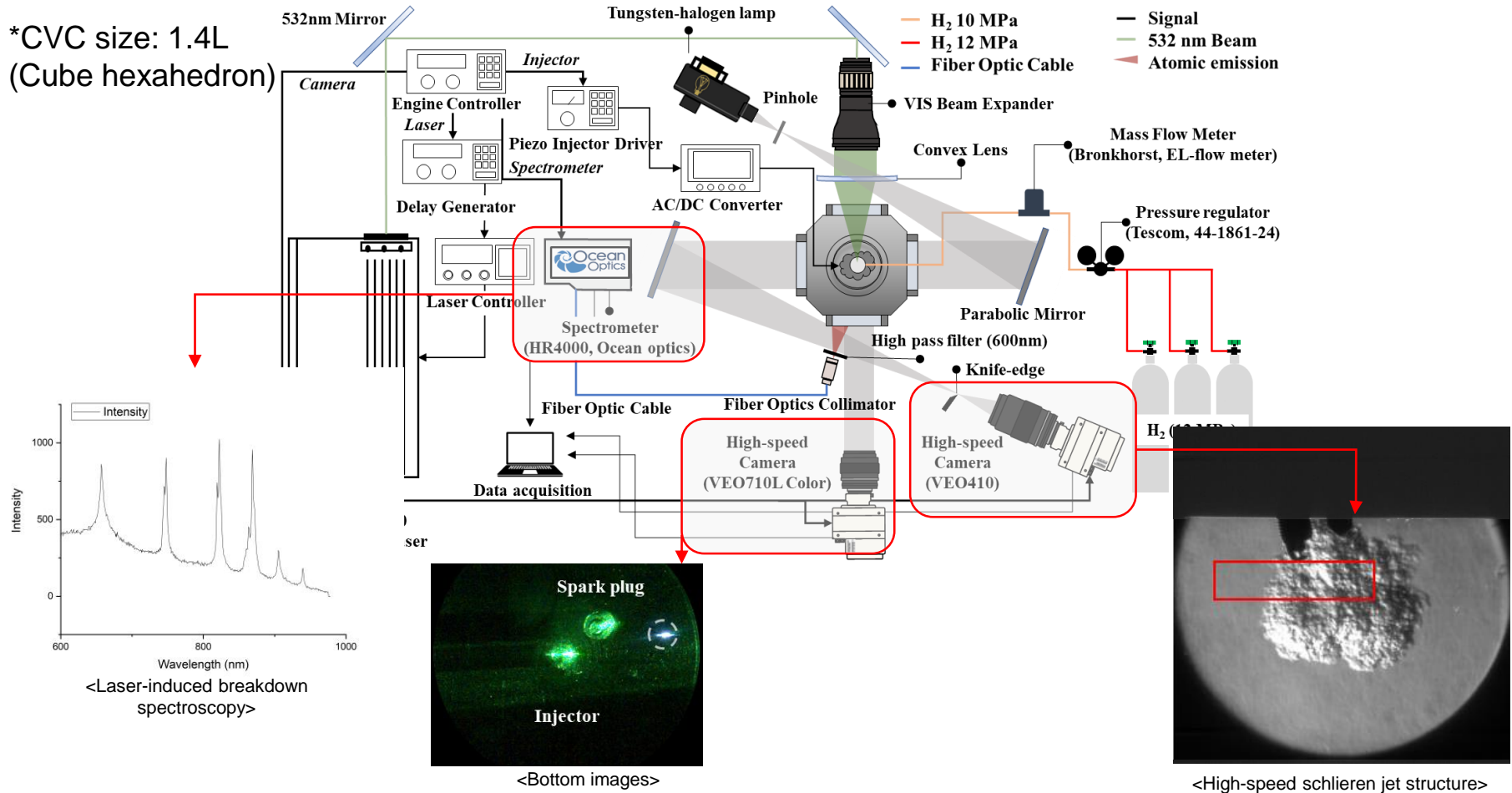
1. Measure the local equivalence ratio of homogenous/stratified hydrogen mixture using *LIBS methodology
2. Define hydrogen jet shape created by hollow-cone injector
3. Obtain mixture flammability by examining local equivalence ratio
4. Observe spark plug arc discharge channel ignitability.



Experimental Setup (Schlieren & LIBS) in CVCC

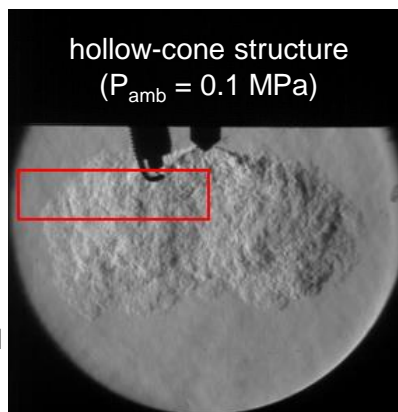
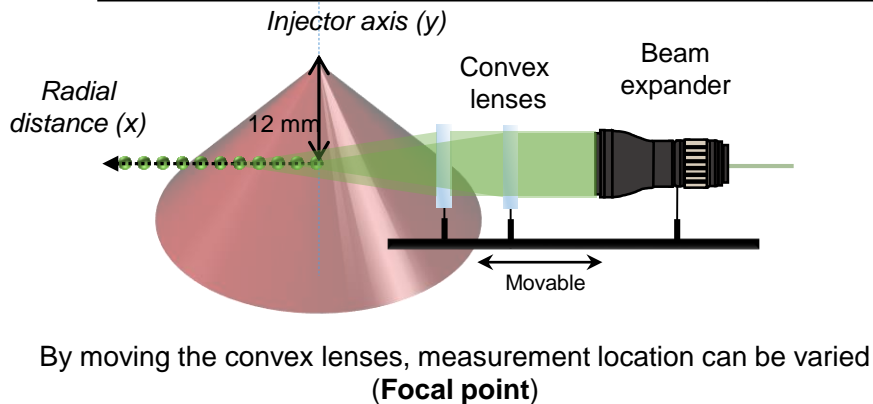
*CVCC: Constant Volume Combustion Chamber

*CVC size: 1.4L
(Cube hexahedron)

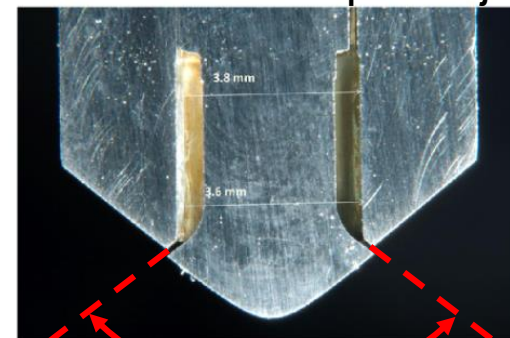


- LIBS under different ambient pressure / measurement location

| Parameters | Values |
|---|---|
| Injection duration [ms] | 1 |
| Ambient / hydrogen temperature [K] | 323.0 |
| Injection pressure [MPa] | 10.0 |
| Ambient pressure [MPa] | 0.1, 0.5, and 1.0 |
| Measurement location from injector tip (x) [mm] | 3 – 32 (non-linear) *Fixed vertical location |



Hollow-cone shaped Injector

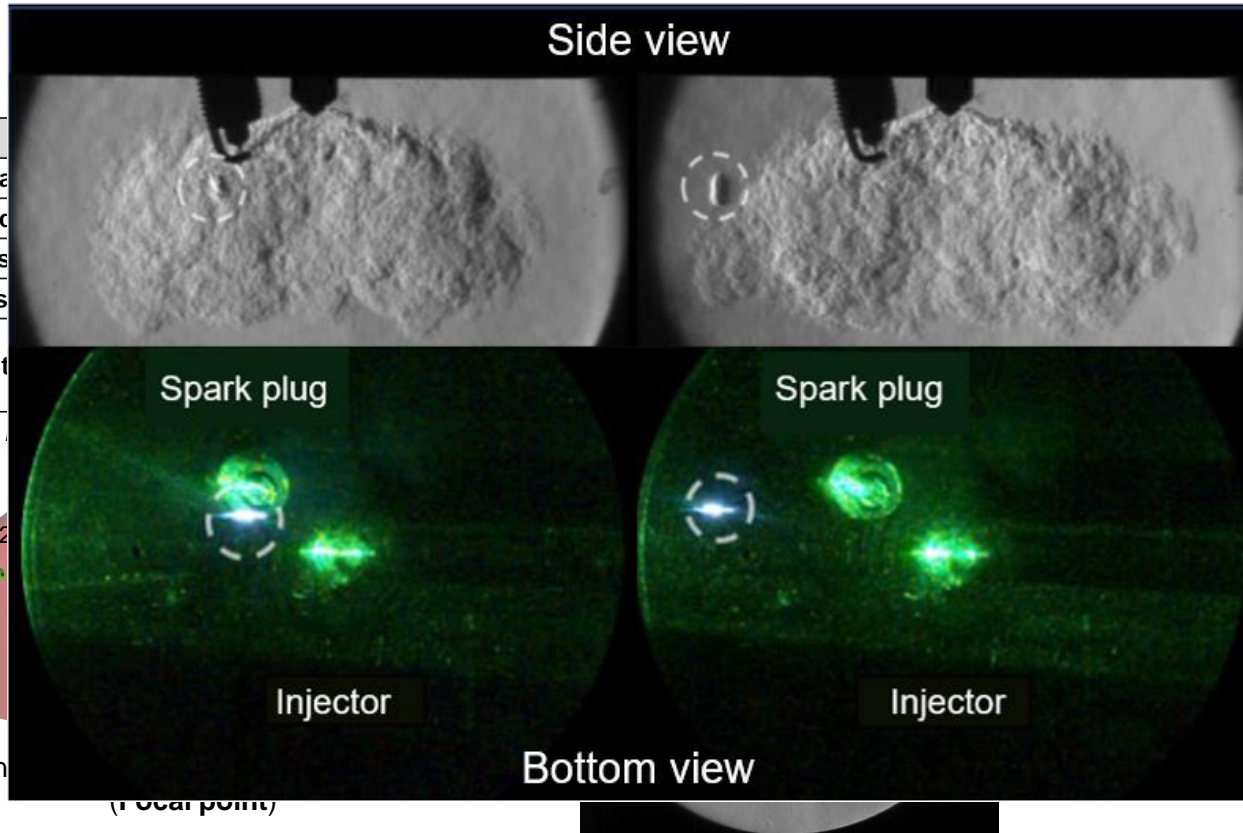


94°

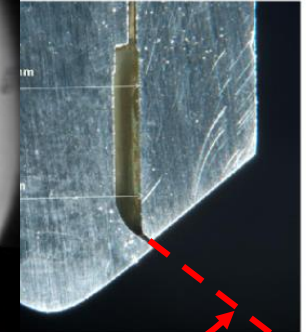
- Hollow-cone shaped injector creates a **hollow-shaped hydrogen jet**

Experiment Conditions

- LIBS under different ambient pressure / measurement location



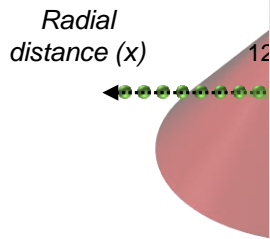
one shaped Injector



94°

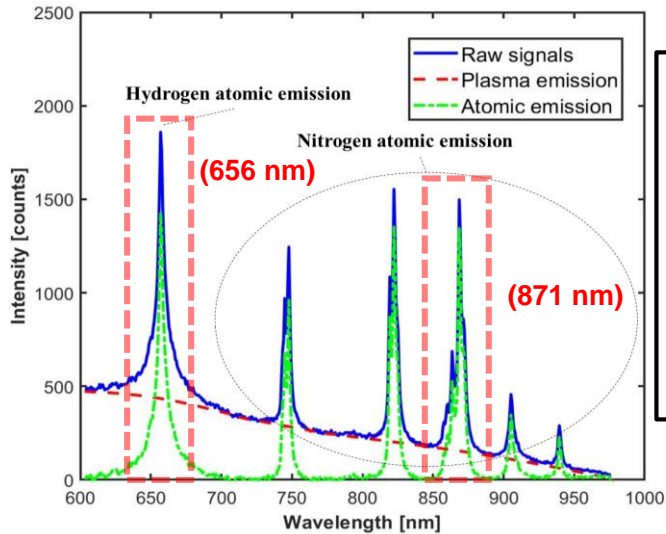
one shaped injector
a hollow-shaped
in jet

| |
|----------------|
| |
| Injection dura |
| Ambient / hyc |
| Injection pres |
| Ambient pres |
| Measurement |



By moving the con

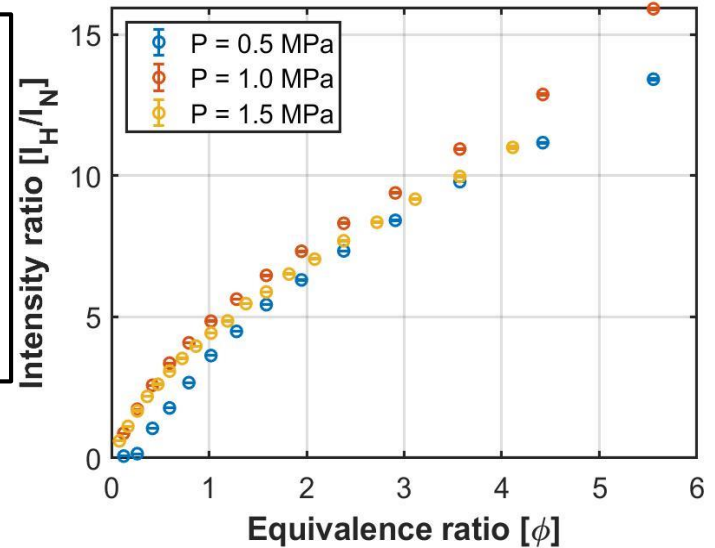
(focal point)



<Post-processed spectrometer signals>

- Post-Processing data = Raw Data – Background
- Removing background → improve the SN ratio
- **Hydrogen and Nitrogen Intensity ratios are constant**
- Calibration process (based on the ideal gas law)

With 200 times repetition

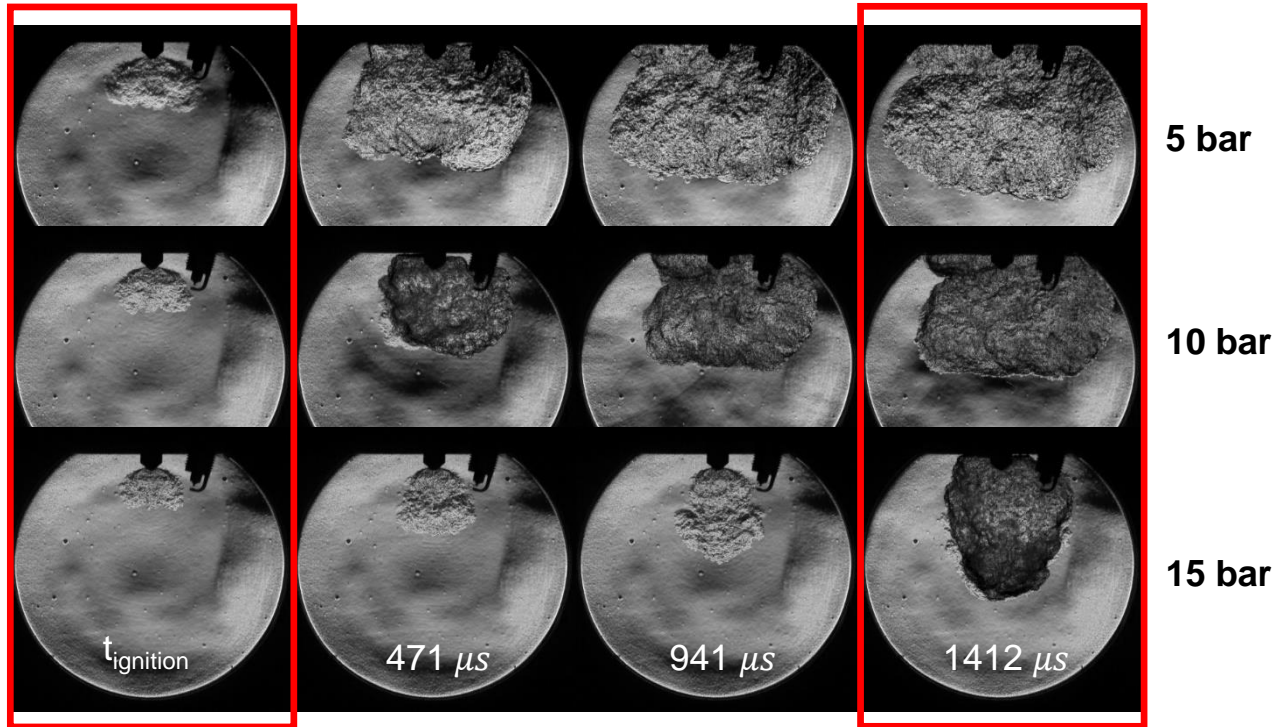


$$\text{Equivalence ratio } (\Phi) = \alpha \left[\frac{I_H}{I_N} \right]^2 + \beta \left[\frac{I_H}{I_N} \right]$$

Where, α, β = empirical constant,
 I_H = Intensity of hydrogen atomic emission [counts]
 I_N = Intensity of nitrogen atomic emission [counts]

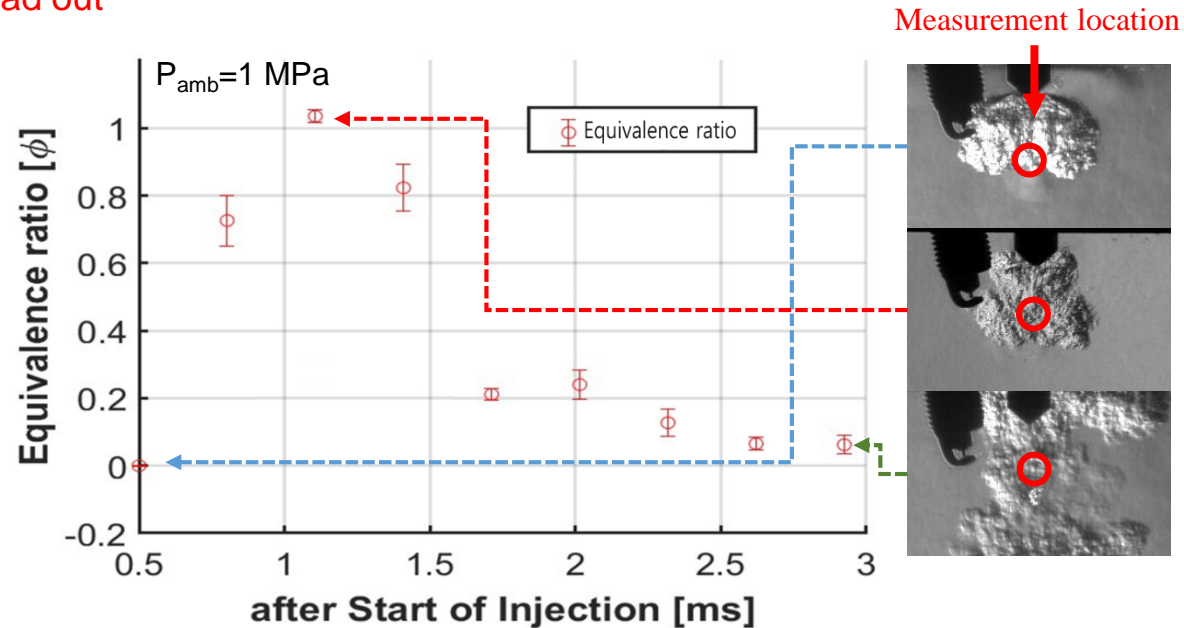
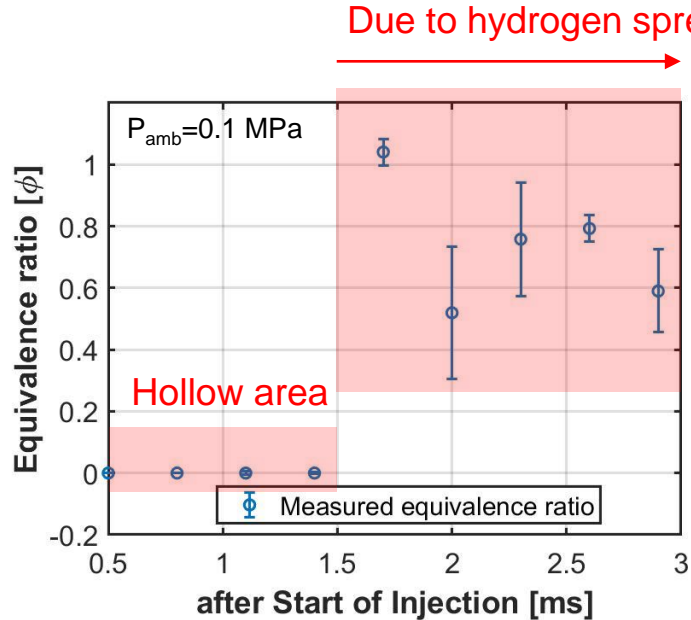
Hydrogen Jet at Various Ambient Pressure

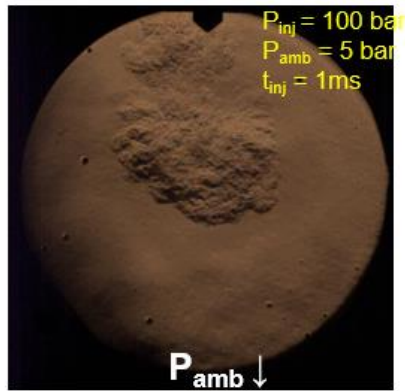
Hydrogen Stratified Combustion: Local equivalence ratio varies combustion characteristics



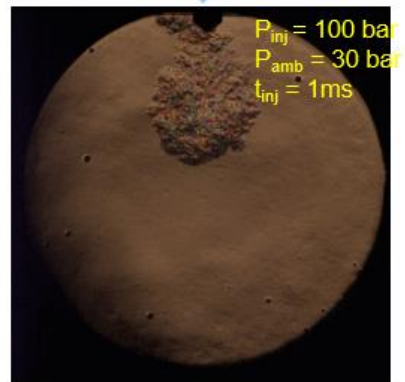
- At high atmospheric pressure, **jet is contracted** so that hydrogen does not reach the spark plug directly .
- It is assumed that the increase in the atmospheric pressure is the main cause for the contracted jet shape (Spatial effect)
 - Atmospheric Pressure Increase \rightarrow **Flame Area Reduction**

- High ambient pressure makes the hydrogen move toward inner side of the jet structure
 → jet collapse

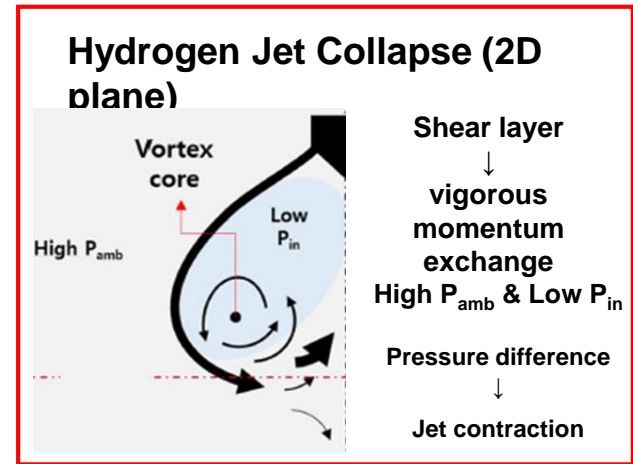
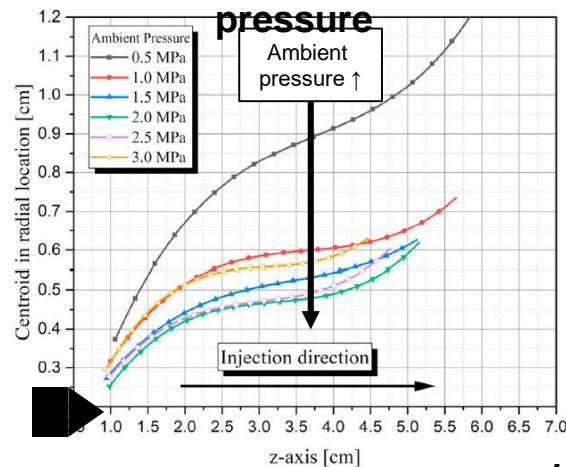




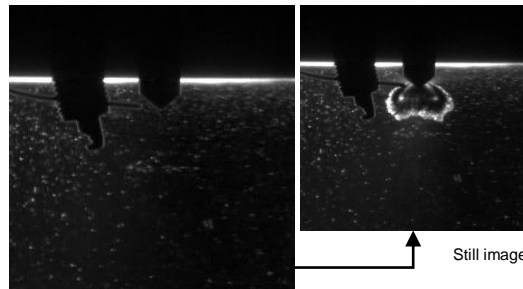
Ambient pressure ↑



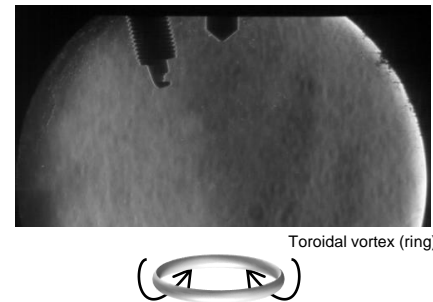
Hydrogen jet contraction according to atmospheric pressure



• High-speed schlieren imaging

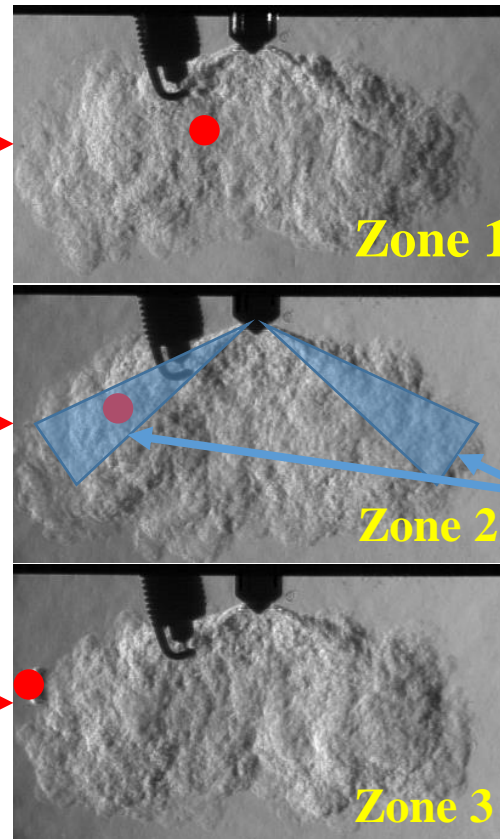
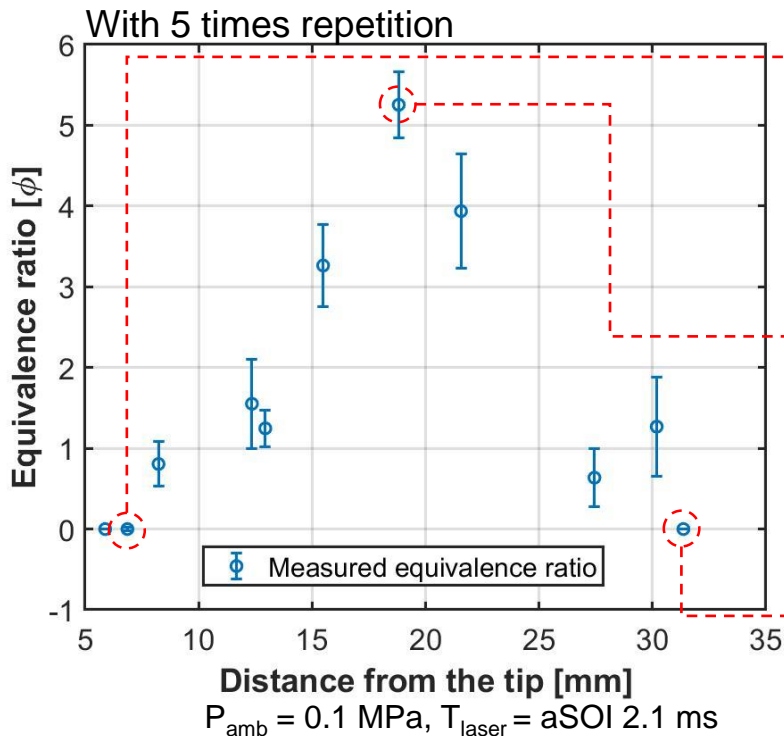


• High-speed shadow imaging



Despite hydrogen having a high diffusion rate, it is observed that **jet shape collapses and contracts** easily under high atmospheric pressure conditions due to **low jet stiffness**.

- Measurement location



Zone 1:
 Due to the hollow area,
 hydrogen was not
 detected

Zone 2:
 Max equivalence ratio
 was observed;
Jet center core region

Zone 3:
 Hydrogen was not
 detected at the outer
 side of hydrogen jet
 structure

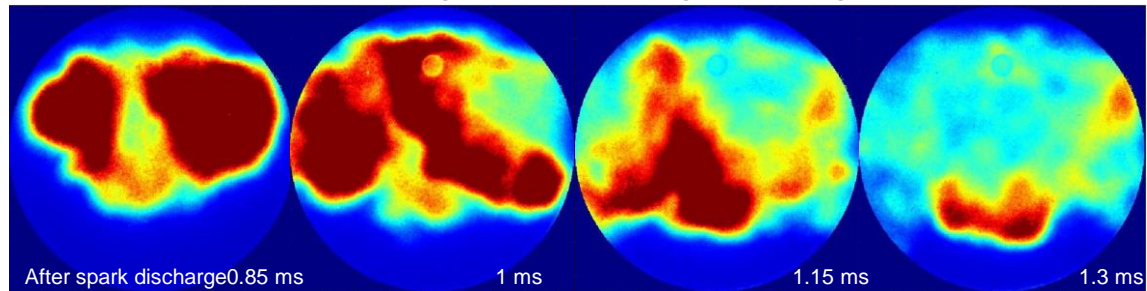
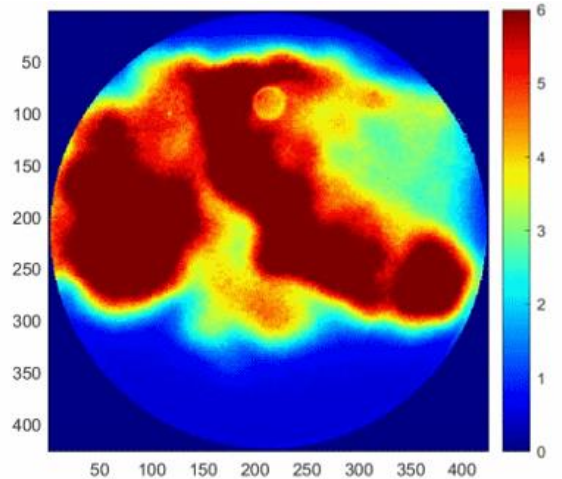
- Measured Equivalence Ratio Corresponds to the Results of Captured Hydrogen Jet Images

Hydrogen Energy Conversion ($P_{amb}=0.1$ Mpa, $p_{inj}=10$ Mpa)

- OH chemiluminescence indicated local-rich mixture when the ignition discharged during the injection

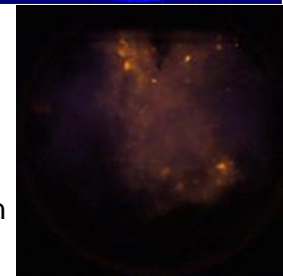
*ignition discharge during injection

(a.u.)

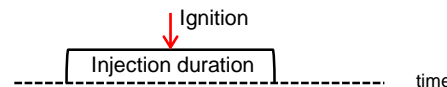


: Because the injection was still made after the ignition discharge, high OH intensity was measured at the center of optical window.

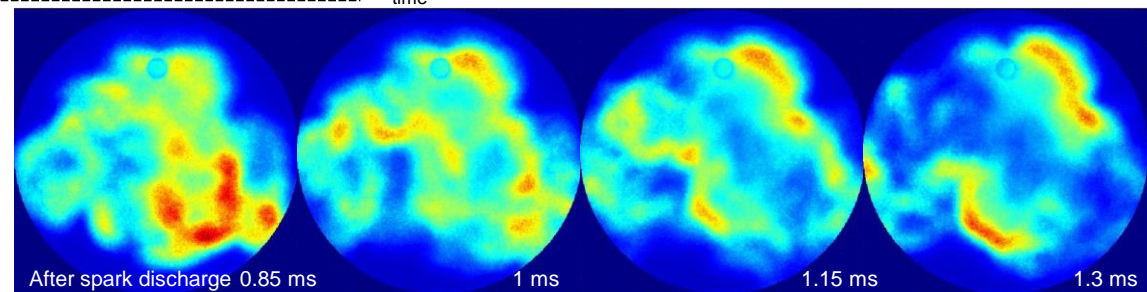
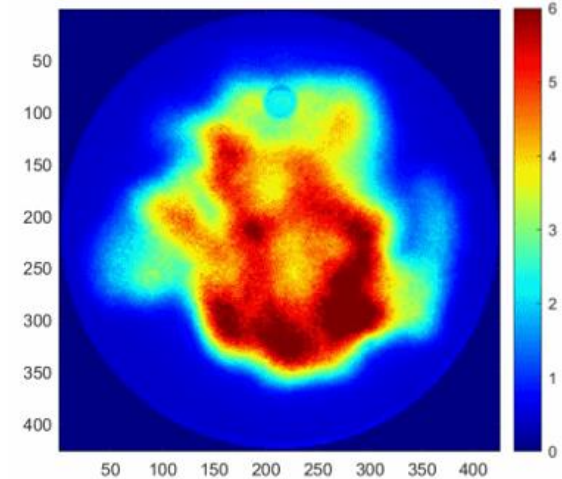
*Direct flame visualization



OH chemiluminescence results (ASOI: 1024 μ s)



*ignition discharge after the end of injection (a.u.)



: Mixture is rather lean and more distributed, but the local-rich area still exists

*Direct flame visualization



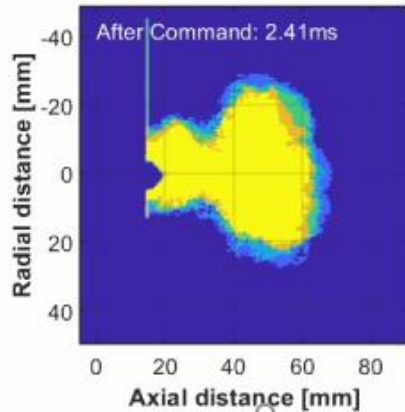
OH chemiluminescence results (ASOI 2560 μ s)



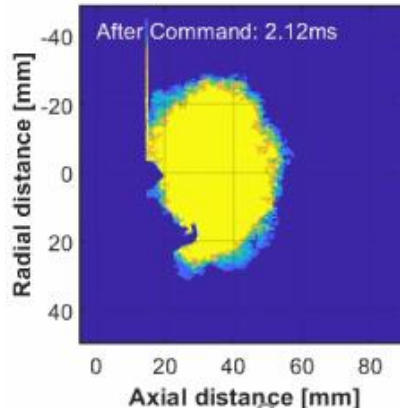
Double injection w.r.t. split ratio

- Jet structure change depending on split ratio ($P_{amb} = 5 \text{ bar}$, dwell time = $600\mu\text{s}$)

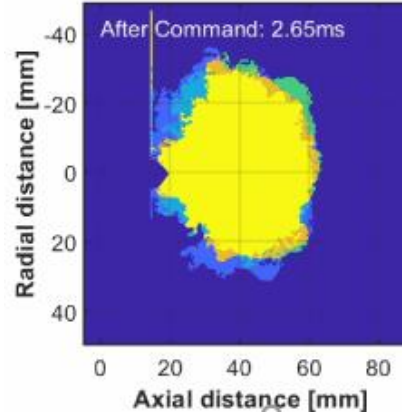
Single



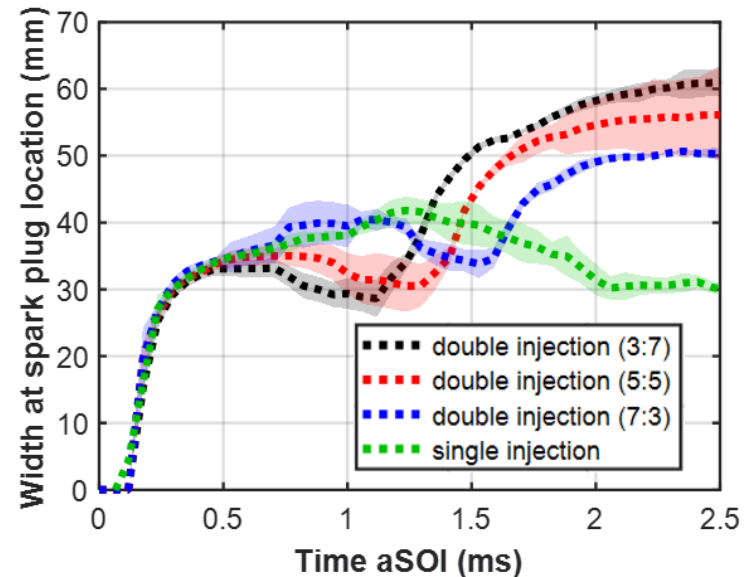
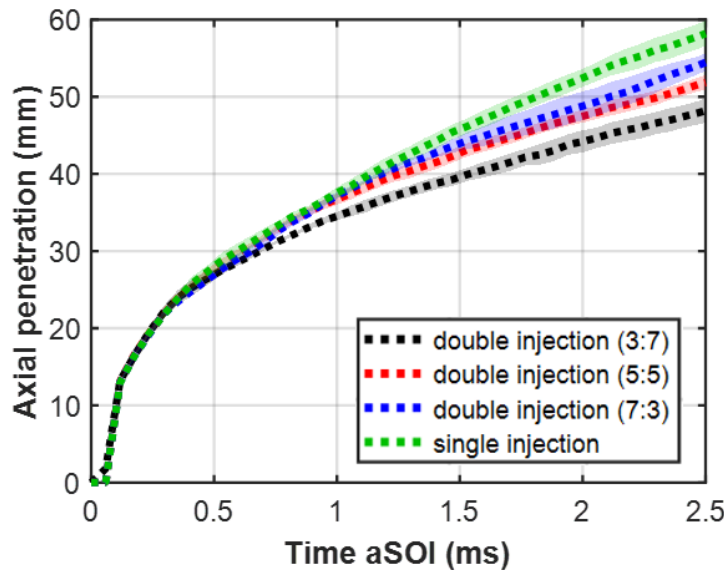
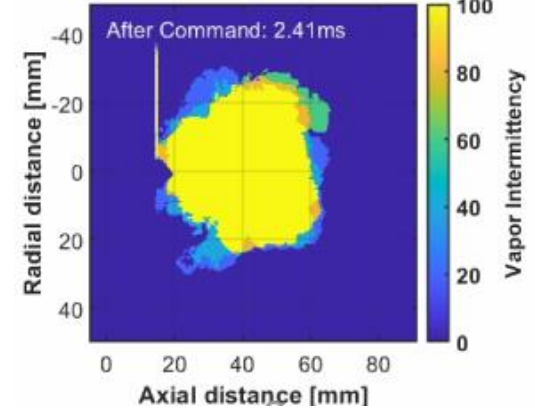
Split ratio 3:7



Split ratio 5:5



Split ratio 7:3

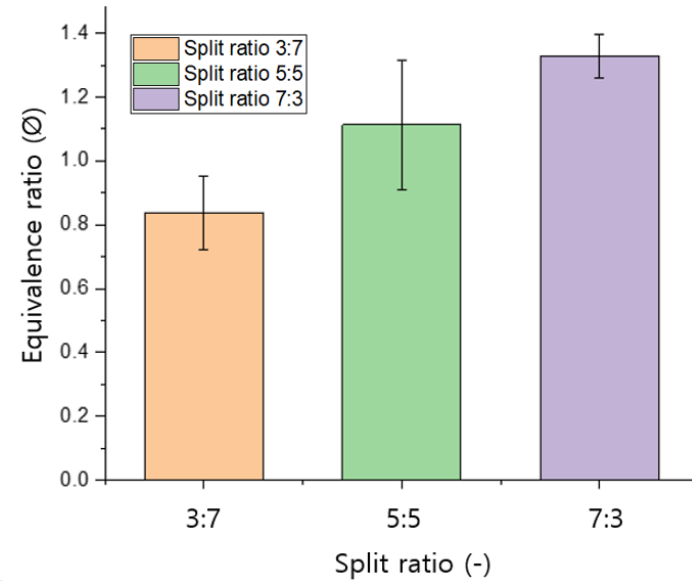
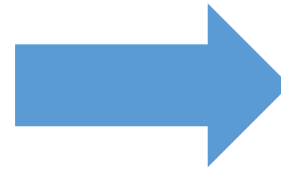
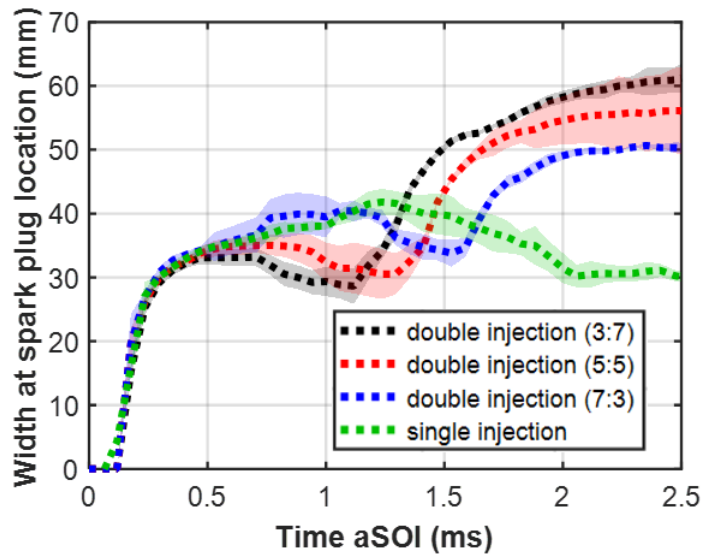
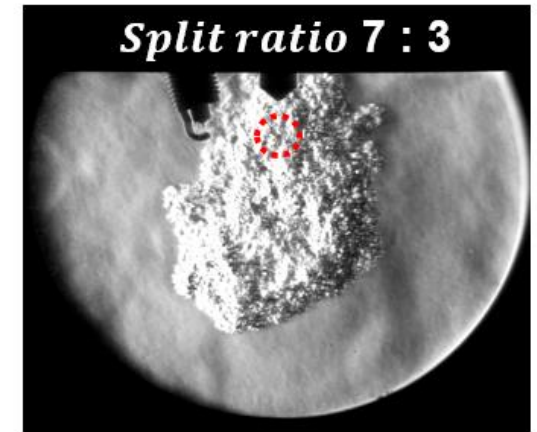
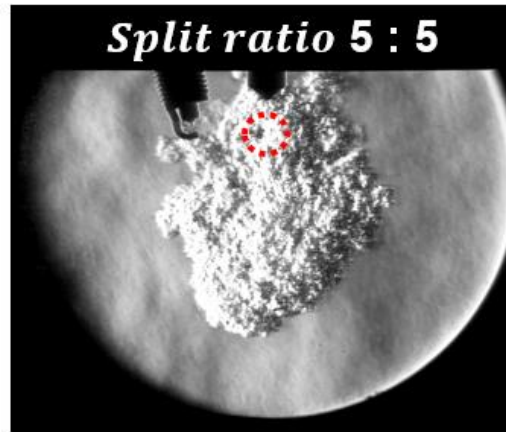
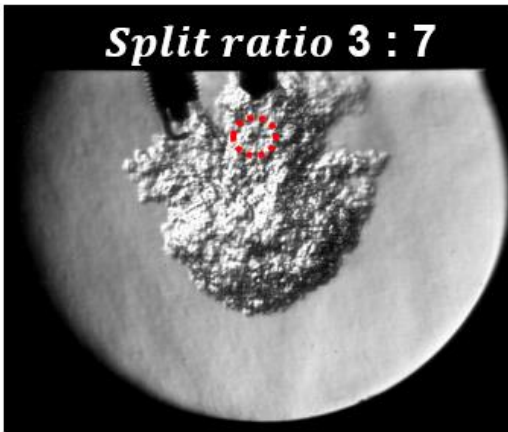


For double injection, hydrogen jet spread out to spark plug penetration, but penetration was decreased
 → Increases in 2nd injection portion caused jet dispersion after end of the 2nd injection

Double injection w.r.t. split ratio

- Local equivalence ratio measurement

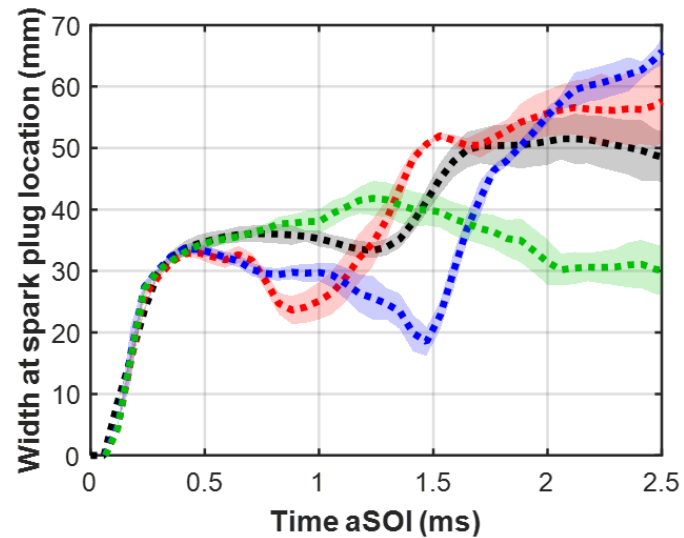
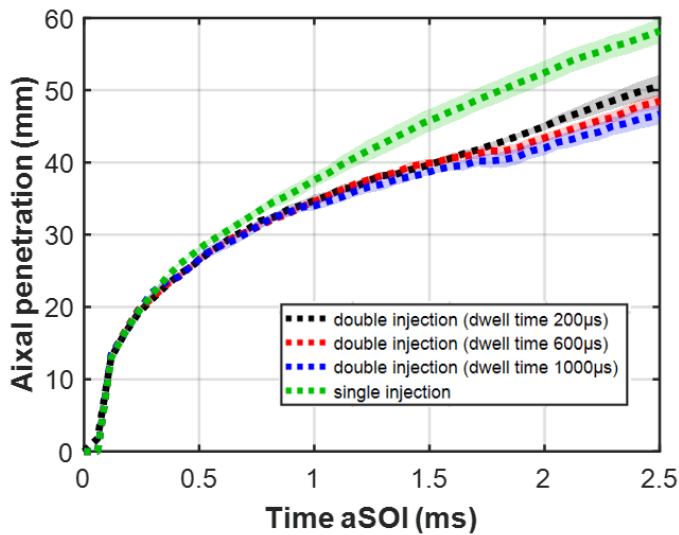
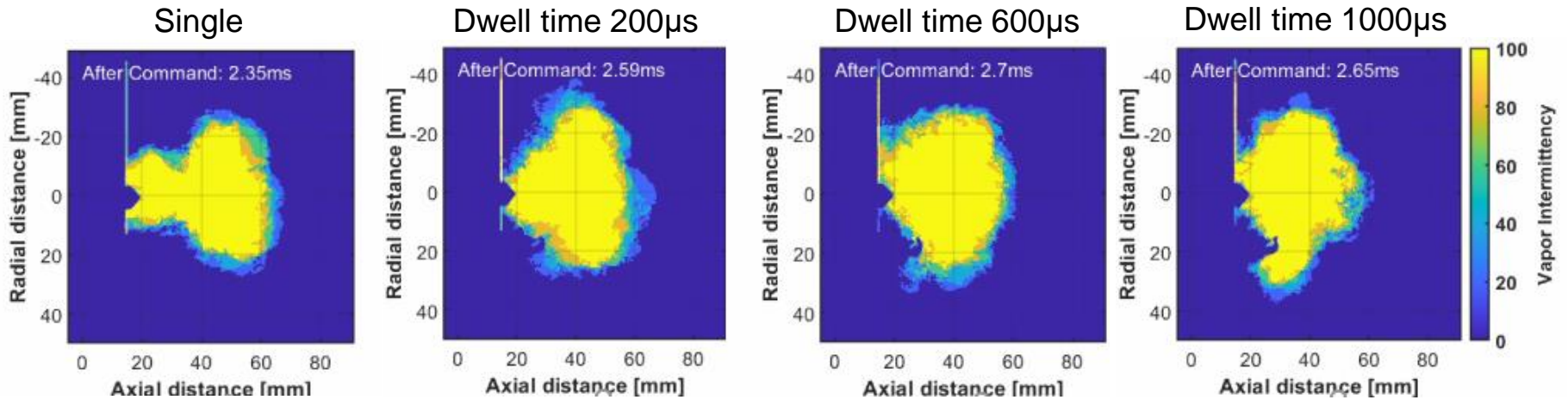
- Changes in local equivalence ratio depending on split ratio ($P_{amb} = 5 \text{ bar}$, dwell time = $600\mu\text{s}$)



Dispersion of jet meant that jet was moving outward \rightarrow Low hydrogen concentration at jet center
 \rightarrow Lower local equivalence ratio measurement at the center

Double injection w.r.t. dwell time

- Jet structure change depending on dwell time ($P_{amb} = 5 \text{ bar}$, split ratio = 3:7)

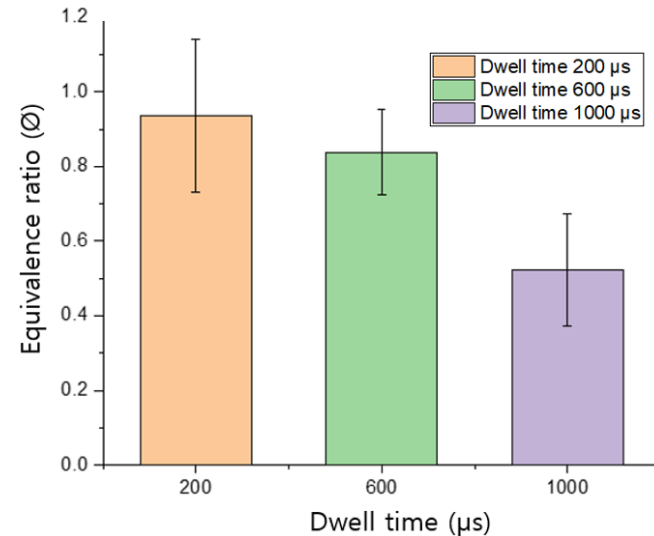
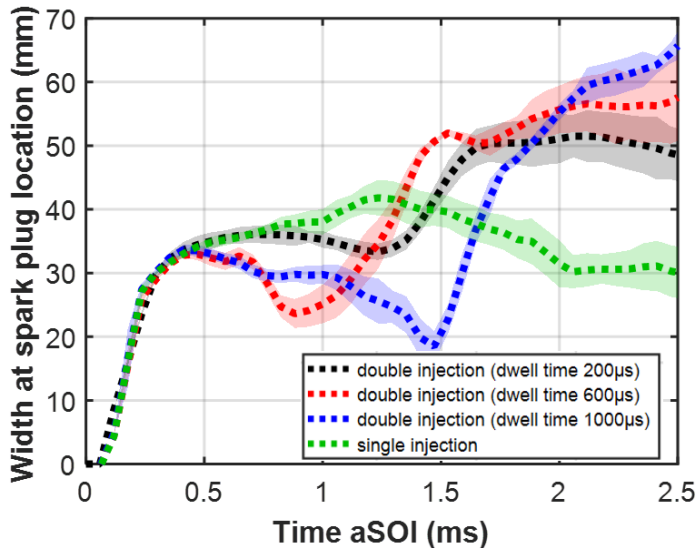
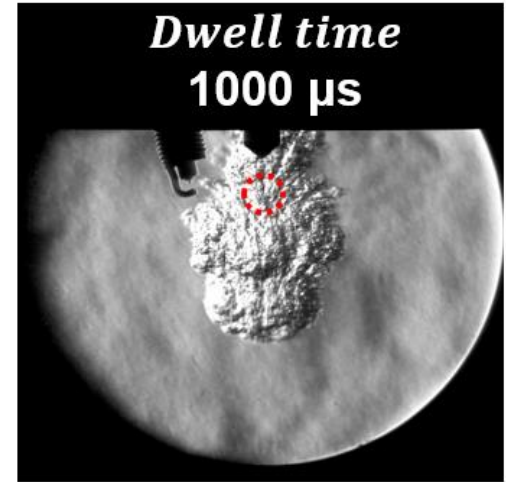
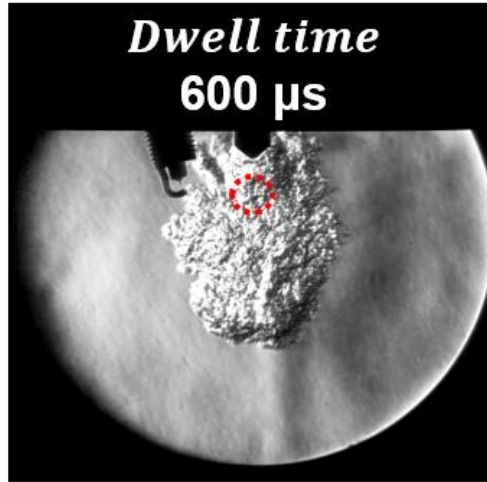
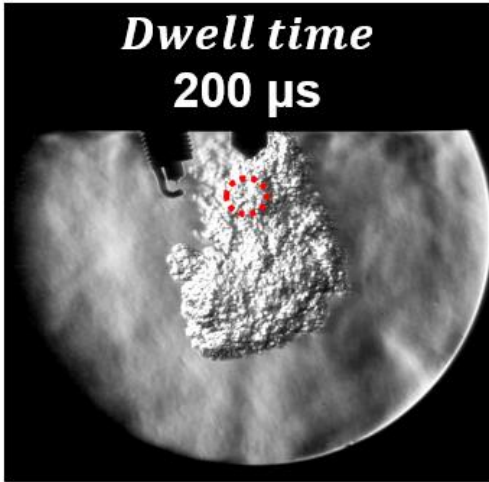


Although the change in penetration was limited depending on dwell time, jet width changed substantially
 → Increases in dwell time caused higher hydrogen dispersion

Double injection w.r.t. dwell time

- Local equivalence ratio measurement

- Effect of dwell time on the hydrogen jet equivalence ratio ($P_{amb} = 5 \text{ bar}$, Split ratio = 3:7)

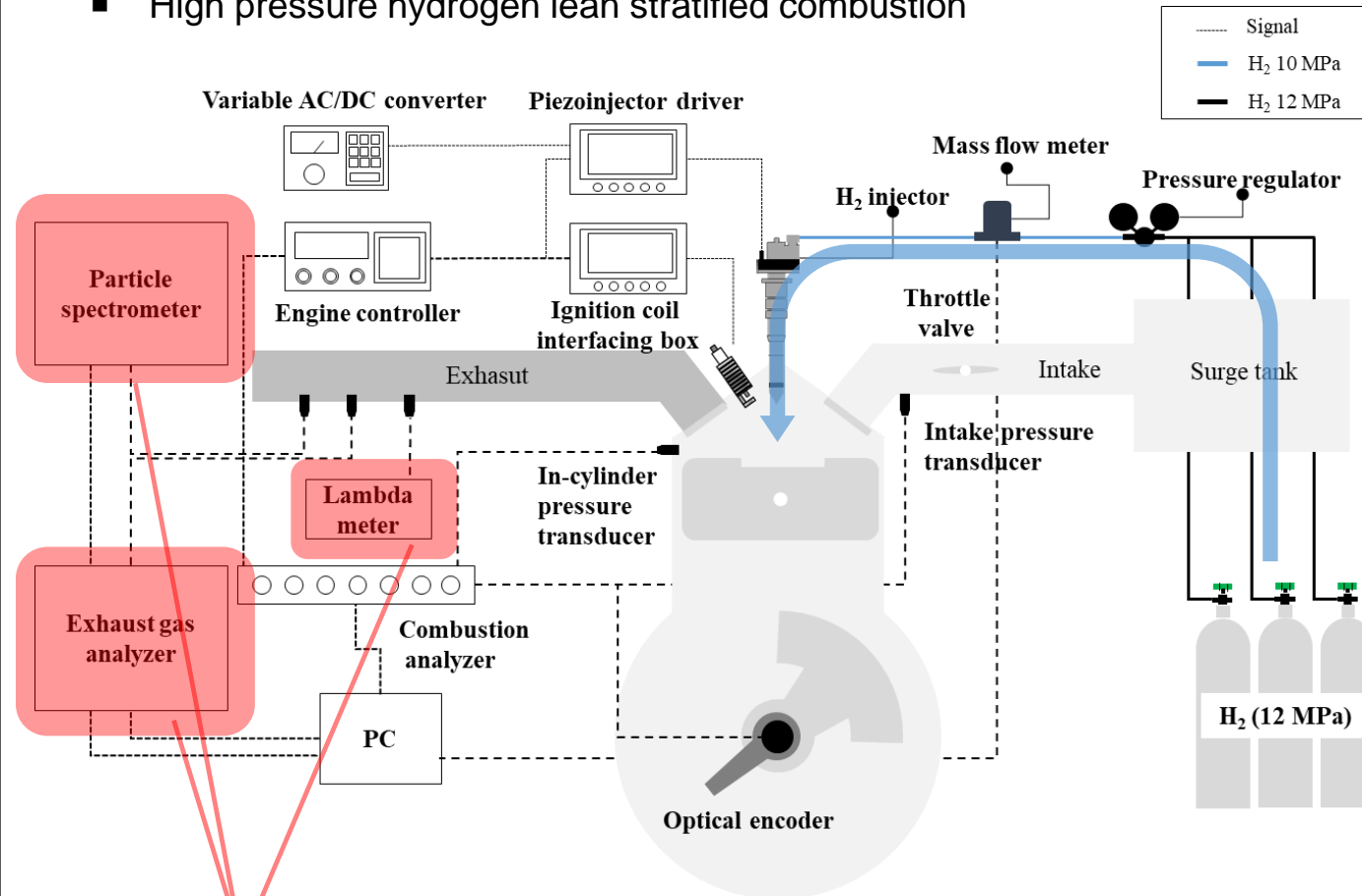


At dwell time = 200 μs , hydrogen concentration at the jet center was increased (higher ϕ)

At dwell time = 1000 μs , hydrogen dispersion was increased and concentration at the center was decreased (Lower ϕ)

Experimental Setup for Single Cylinder Engine

- High pressure hydrogen lean stratified combustion

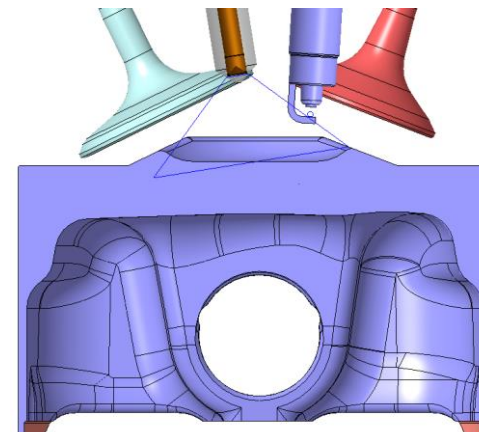


- Experiment schematic of hydrogen reciprocating engine

- PM & NO_x emission
- Air ratio(λ)

| Parameters | Values |
|-------------------|---------------------------------------|
| Engine type | Spray guided Spark ignition DI engine |
| Bore X Stroke | 85 X 88 mm |
| Compression ratio | 12: 1 |
| Intake valve | 11 aTDC – 22 aBDC |
| Exhaust valve | 34 bBDC – 10 aTDC |
| Injector | Outwardly opening piezo injector |

*Reciprocating engine head



Experimental Conditions

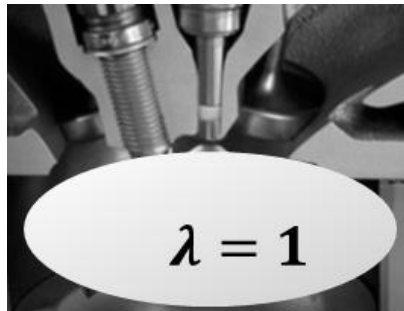
- Experimental conditions for single-cylinder research engine
- Effect of ignition timing on hydrogen SCC
- Effect of mixture formation mode on the combustion and emission characteristics

| Parameters | Value |
|--------------------------------|---------------|
| Engine speed | 1300 rpm |
| Injection pressure | 10 MPa |
| Injection quantity | 160 g/h |
| Throttle valve position | 0 % (WOT) |
| Air excess ratio (λ) | 2.5 |
| Injection timing (t_{inj}) | 32 bTDC* |
| Ignition timing (t_{ig}) | -12 – 18 aTDC |

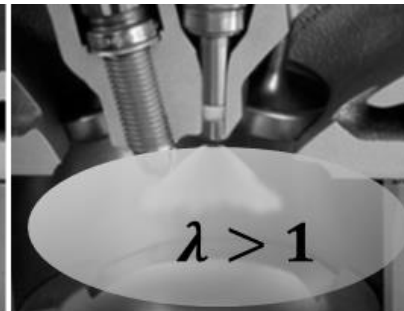
| Parameters | Homogeneous charge | Lean homogeneous charge | Lean-stratified charge |
|----------------------------------|--------------------|-------------------------|------------------------|
| Engine speed | 1300 rpm | | |
| Injection pressure (P_{inj}) | 10 MPa | | |
| Injection quantity | 188 g/h | | |
| Throttle valve position | 98 % | 92 % | 0 % (WOT) |
| Air excess ratio (λ) | 1 | 1.7 | 2.3 |
| Injection timing (t_{inj}) | 158 bTDC | 158 bTDC | 26 bTDC |



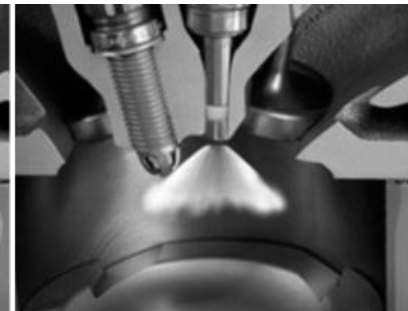
Lean-stratified charge ($\lambda = 2.3$)



Homogeneous charge ($\lambda = 1$)



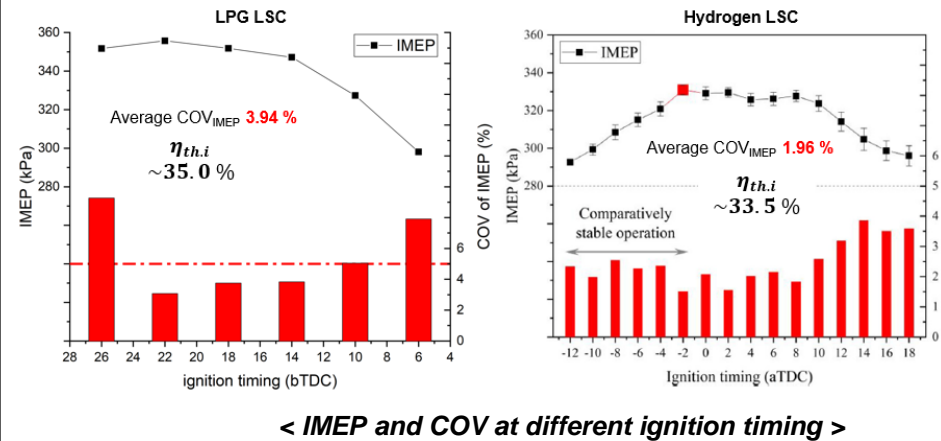
Lean homogeneous charge ($\lambda = 1.7$)



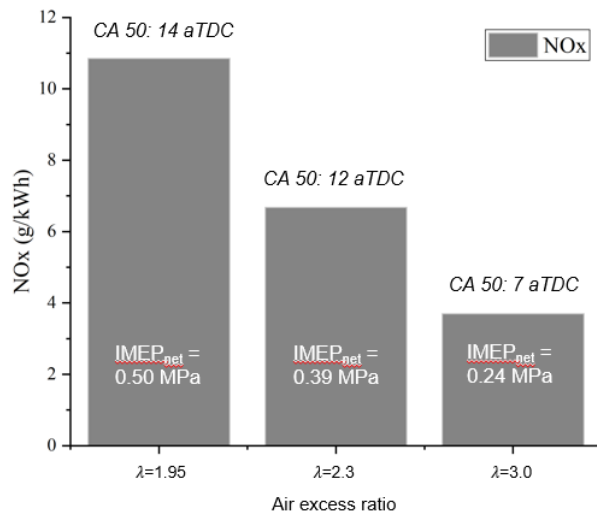
Lean-stratified charge ($\lambda = 2.3$)

*Average value of 300 cycles

*Use only under COV_{IMEP} 5 % data



- In the case of hydrogen, **Stable operation within wide mixture area** (Overall low COV_{IMEP} measured)
- In the case of hydrogen, the process required for phase change such as atomization and evaporation is not required, so **stable ignition is possible** immediately after injection is terminated
- **Low indicated thermal efficiency** result than LPG stratified combustion (Estimated to be due to heat transfer loss)

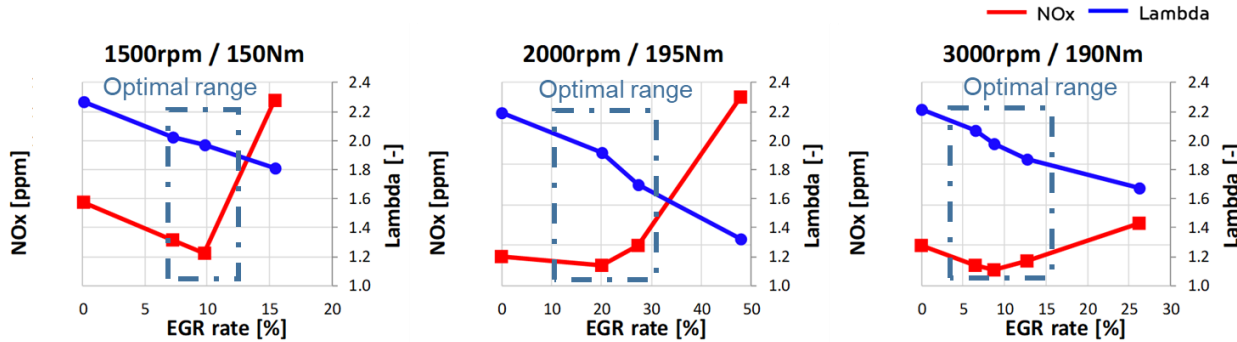


< Results of NOx emission by air excess ratio (MBT timing) >

- Lower NOx emissions as air excess ratio increases
- Confirm the possibility of reducing NOx emissions through stratification (ex. Lean-boosting, e-turbo)

Effect of EGR in a hydrogen prototype engine

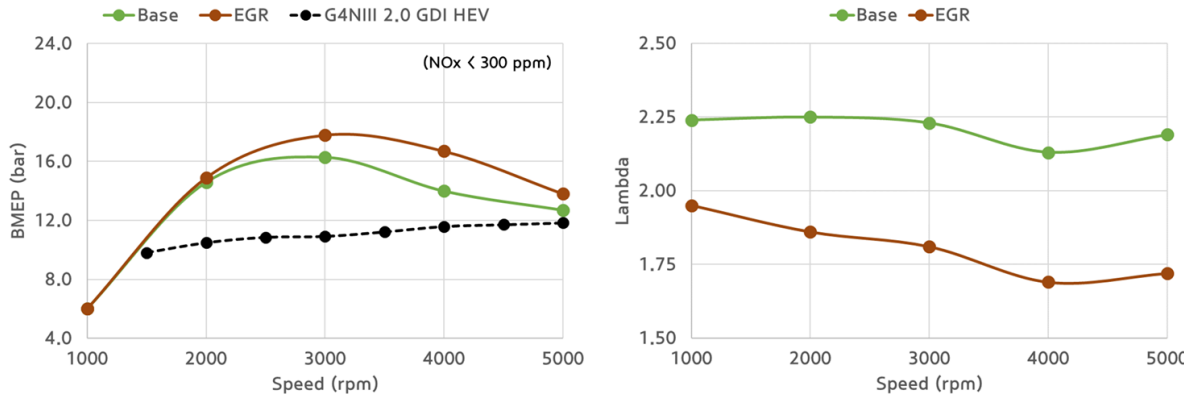
■ NOx Trend and AFR Changes



- **NOx reduction by increasing EGR supply** → Increasing H₂ amount
→ possible to improve engine performance

- Optimal EGR rate for each engine operating condition
- **Maximum NOx reduction when 10 ~ 20 % of EGR**
- NOx increased when more EGR rate than optimal rate

■ WOT Performance with EGR

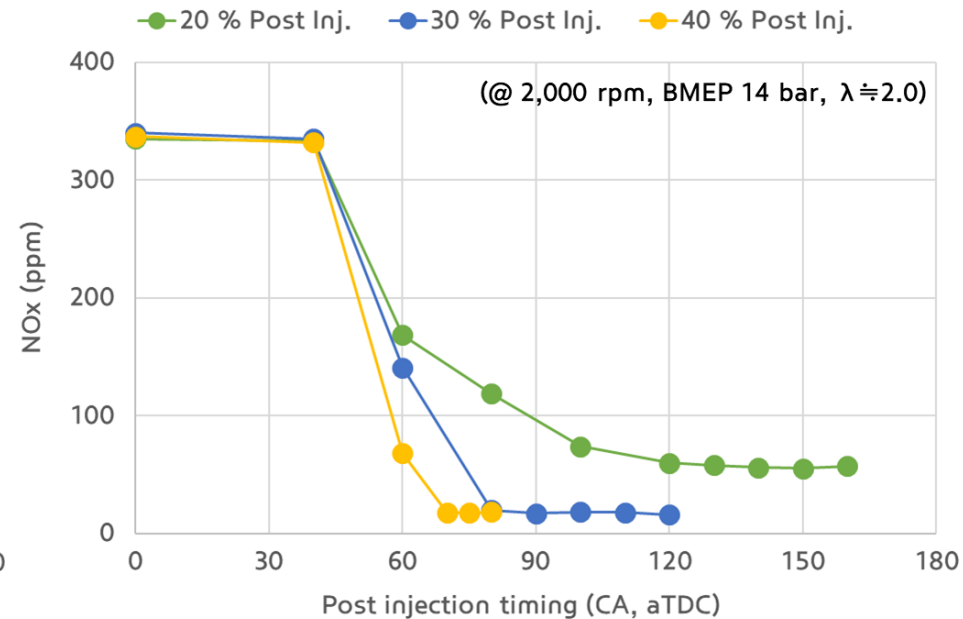
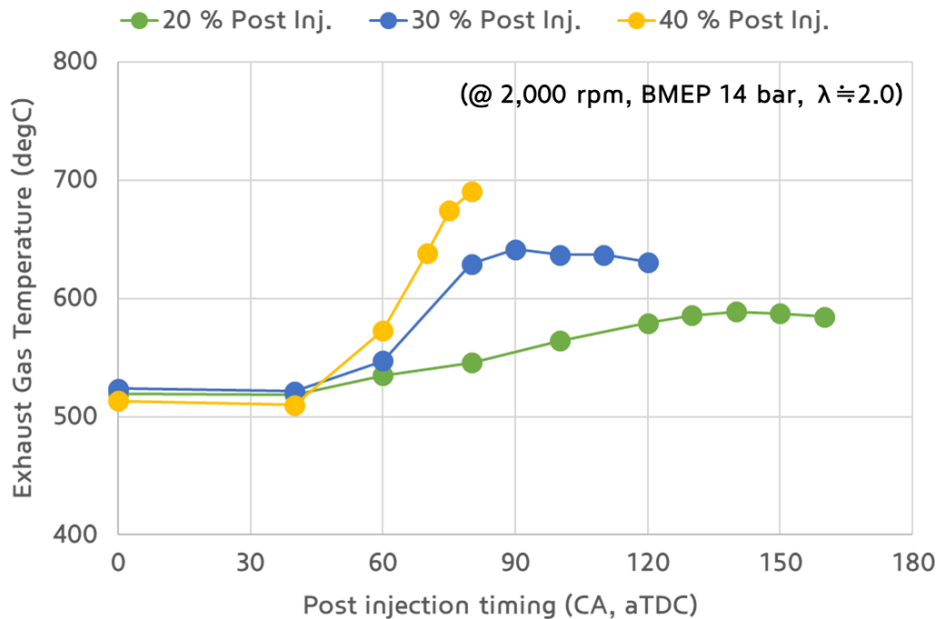


- **AFR could be reduced by supplying EGR while maintaining NOx limit**
→ Increasing the amount H₂ supply
→ Better WOT performance (Max. 13 % under mid-high speed range)

Source: R&D Technology Forum : Sustainable Carbon neutral ICE, Hyundai Motor Company, 2023

Effect of Post-Injection with ATS

Exhaust Gas Temp. and NOx Trend (@ 2,000 rpm/BMEP 14 bar)



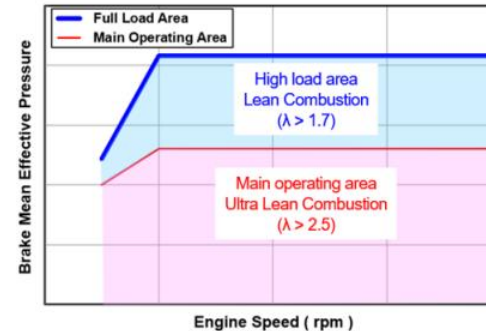
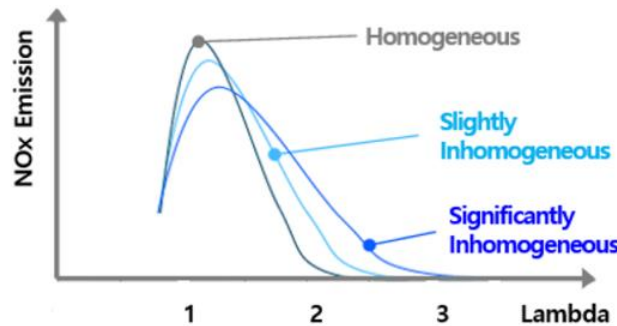
- The more injection amount and the later injection timing of post-injection, the **higher exhaust gas temperature and the lower NOx** (@ same AFR, same BMEP)

→ Possible to improve engine power by lower AFR or reduce of aftertreatment system complexity when post-injection is applied

Source: R&D Technology Forum : Sustainable Carbon neutral ICE, Hyundai Motor Company, 2023

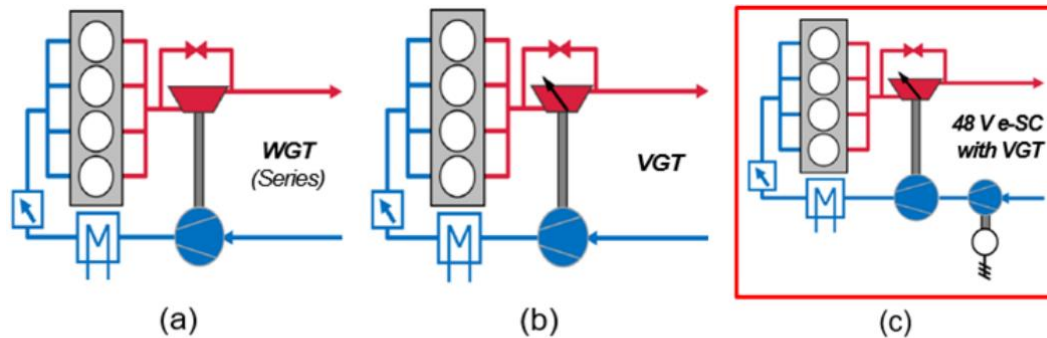
Target engine and development concept Boosting System

- It was found through previous researches that near zero NOx emission is possible when $\lambda > 2.5$, but NOx emission is highly dependent on mixture homogeneity.
- For high load, target is to achieve $\lambda > 1.7$ to prevent abnormal combustion.



NOx emission ratio (left), excess air ratio target

- Two-stage boosting system combining 48 V driven electric supercharger & VGT is implemented.



WGT (a), VGT (b), 2-Stage boosting system (c)

- Hydrogen ICEV has a better feasibility than BEV or FCEV because of its lower TCO and low dependence on rare earth material.
- Hydrogen ICE has a similar engine performance to conventional fossil fuel while maintaining lower NO_x emission.
- LIBS can measure the local equivalence ratio of the hydrogen mixture.
- Delaying ignition timing increased the homogeneity of the stratified mixture.
- Double injection can modify the hydrogen jet behavior in terms of penetration and width → reduce the jet contraction at high ambient pressure.
- Hydrogen ICE is free from CO₂ and has a wider flammable range compared to fossil fuel.
 - Air boosting systems such as WGT, VGT, and e-Turbo can improve performance and thermal efficiency.
- EGR should be considered to reduce NO_x emission when produced more while operating an engine under lean stratified charge mode compared to lean homogeneous charge mode.



Thank you for your kind attention.

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